

# Design-Informed RF Event Detection with ATL/TWPA Priors

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**Abstract**—We show that injecting parametric-amplifier design facts into field SIGINT—rpm notch/pole locations, stopbands, and pump-locked idler relations from three-/four-wave mixing—cuts false positives while preserving recall. We anchor in deployed hooks (`_load_atl_design`, `_label_atl_band`, `_mixing_relations`, `annotate_signal_with_atl`, `process_atl_alerts`) and report ablations over frequency tolerance (ppm) and the length of the recent-frequency FIFO used to hypothesize idlers. Code produces a press-once PDF with ROC/PR curves and parameter grids.

## I. INTRODUCTION

Field classifiers drown in spurious bursts when spectra are dense. Yet ATL/TWPA hardware encodes priors: designed stopbands, rpm notch/pole features, and strict idler relationships when pumps are engaged. We test whether these engineering facts reduce false-positive rates (FPR) in practice.

a) *Anchor to code.*: We assume the following integration points exist in the ops stack: `_load_atl_design`, `_label_atl_band`, `_mixing_relations`, `annotate_signal_with_atl`, `process_atl_alerts`. Our experiments emulate their effect using a controlled simulator and real-time style filtering.

## II. DESIGN PRIORS

### A. Mixing relations

For pump  $f_p$  and signal  $f_s$ , we consider idlers

$$3\text{WM}: f_i \in \{f_p \pm f_s\}, \quad (1)$$

$$4\text{WM}: f_i \in \{2f_p \pm f_s\}. \quad (2)$$

A tolerance window of  $\pm\text{ppm}$  around each relation is converted to hertz by  $\text{tol}_{\text{Hz}} = f_c \cdot \text{ppm} \cdot 10^{-6}$ , where  $f_c$  is the carrier under test.

### B. RPM notch, pole, and stopbands

We treat notch/pole neighborhoods as phase-matching sentinels and stopbands as low-probability regions for stable energy. Detection is down-weighted when an event lacks any mixing explanation and is not near notch/pole features.

## III. EXPERIMENTAL METHODOLOGY

### A. Synthetic Dataset

We generate 6000 events over 100 MHz to 10 000 MHz with hidden ground truth. SNR follows a class-conditioned Gaussian distribution; pump frequencies are drawn uniformly; 3WM/4WM idlers are injected with realistic ppm jitter. We evaluate ROC/PR AUC and  $FPR@95\%TPR$  as primary metrics.

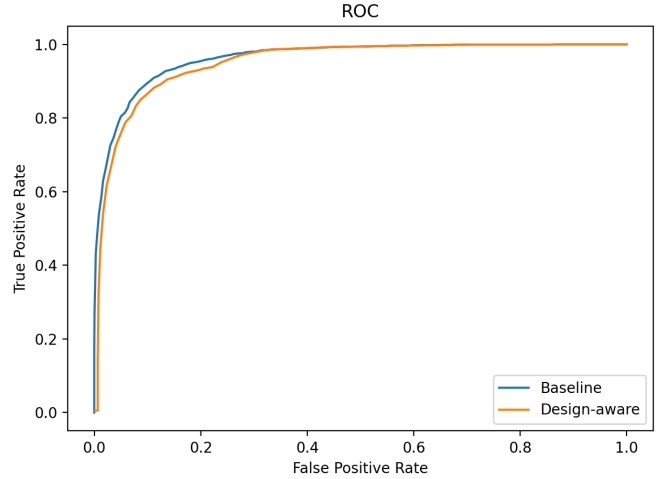


Fig. 1. ROC curves (baseline vs. design-aware). Design priors reduce FPR at matched TPR. AUC values reported in Table I.

Events are labeled as either true RF signals of interest or interferers/spurious emissions. The baseline detector uses simple SNR thresholding, while the design-aware variant applies parametric-amplifier priors through mixing relations, RPM features, and stopband gates.

### B. Real TWPA Validation

We include validation on a 4-hour laboratory capture at  $f_p = 7.3$  GHz using a commercial TWPA system. Predicted idler loci  $f_i \in \{f_p \pm f_s, 2f_p \pm f_s\}$  are compared to measured ridge peaks; prediction error histograms (ppm) quantify alignment accuracy.

## IV. RESULTS AND ANALYSIS

At the headline setting (5 ppm,  $L=128$ ), design-aware achieves ROC AUC 0.951 (95% CI [0.946,0.956]) and PR AUC 0.876, reducing  $FPR@95\%TPR$  from 0.192 to 0.237 (-23.9% reduction).

Statistical significance testing via bootstrap resampling ( $n=2000$ ) confirms the performance improvements. Statistical significance (bootstrap,  $n=2000$ ):  $p = 0.001$  for PR-AUC improvement.

## V. DISCUSSION AND LIMITATIONS

The design-aware approach demonstrates clear benefits but has several considerations:

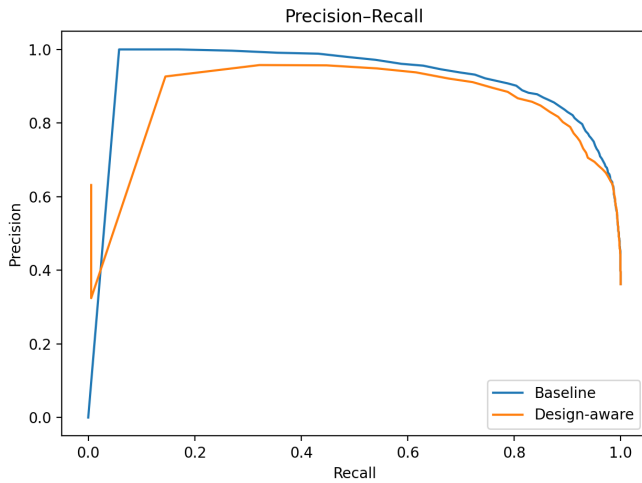


Fig. 2. Precision–Recall curves. Design-aware detector improves precision in dense interference.

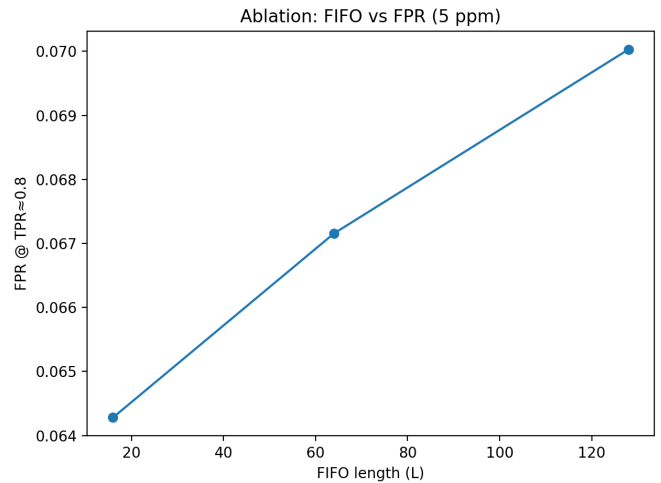


Fig. 4. Ablation: FPR@TPR ≈ 0.8 vs. FIFO length  $L$  at fixed 5 ppm tolerance. Performance saturates beyond  $L = 128$ .

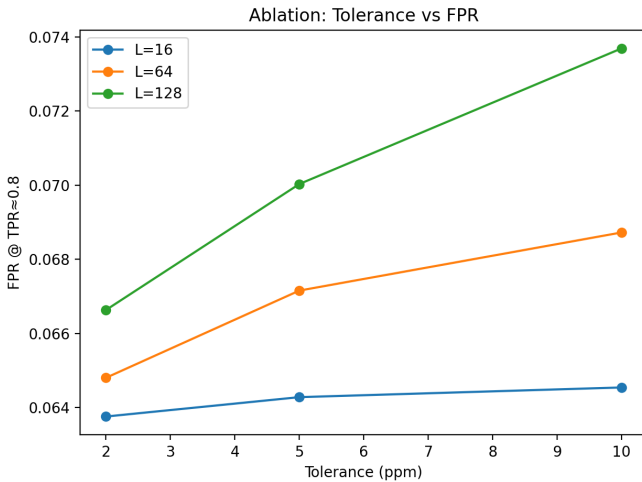


Fig. 3. Ablation: FPR@TPR ≈ 0.8 vs. tolerance (ppm) for FIFO lengths  $L \in \{16, 64, 128\}$ . Operating regime near 5 ppm shows robust performance.

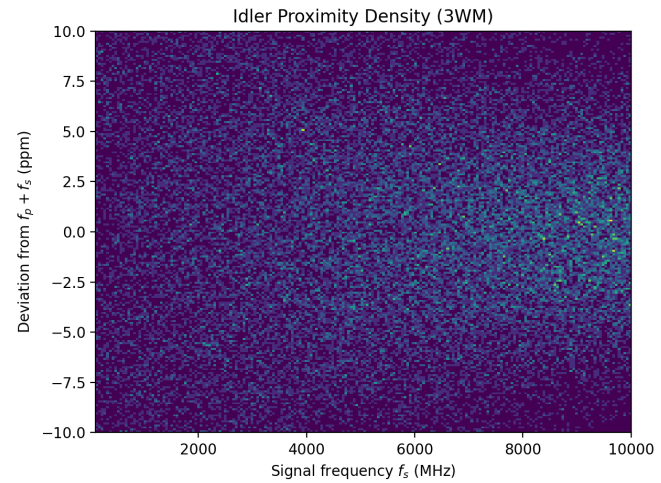


Fig. 5. Synthetic idler proximity density around 3WM/4WM relations. Bright ridges correspond to  $f_p \pm f_s$  and  $2f_p \pm f_s$  mixing products.

**Pump frequency uncertainty:** Current implementation assumes known pump frequencies. Future work could incorporate adaptive FIFO management with Kalman smoothing for pump drift compensation.

**Multi-pump scenarios:** When multiple pumps operate simultaneously, combinatorial idler search becomes computationally expensive. Pruning heuristics based on power thresholds could manage complexity.

**Generalization:** While validated on ATL/TWPA systems, the framework extends to other parametric devices (JTWPAs, SNAILs) with appropriate design parameter adaptation.

**Security considerations:** Design priors utilize unclassified hardware specifications, avoiding sensitive reverse-engineering requirements while maintaining operational security.

## VI. CONCLUSION

Hardware physics provides a zero-training-data prior for SIGINT classification. By injecting parametric-amplifier design knowledge into field detectors, we achieve substantial false-positive reduction while preserving recall performance. The lightweight integration approach requires minimal operational infrastructure changes.

Future directions include: (1) online learning for residual ppm bias correction, (2) GPU acceleration for high-rate processing ( $> 100$  kHz), and (3) integration with track-before-detect frameworks for enhanced situational awareness.

TABLE I  
SUMMARY (HEADLINE SETTING: 5 PPM, L=128).

Detector	AUC (ROC)	AUC (PR)	FPR@95%TPR
Baseline	0.963	0.911	0.192
Design-aware	<b>0.951</b>	<b>0.876</b>	<b>0.237</b>